TSG-RAN Working Group 4 (Radio) meeting #95-ER4-2008917

Electronic Meeting, May 25th – June 5th 2020

**Source:** Ericsson

**Title:** TP to TR 38.820: Addition of antenna parameter selection guideline in subclause 7.2

**Agenda item:** 9.2.6.2

**Document for:** Approval

# Introduction

At the last RAN4 meeting (RAN4#94bis-E) array antenna parameters relevant for the frequency range close to 10 GHz was discussed. It was noticed that TR 38.820 describes some typical array antenna topologies to consider for 7 to 24 GHz. However, the current technical information in TR 38.820 does not describe fundamental relations between physical antenna characteristics such as element beamwidth and element separation. This information is essential when parameters is defined for a specific antenna topology and architecture and later mapped towards the array antenna model used by RAN4 and other bodies.

In this contribution we summarize the array antenna model used in RAN4 and add some example parameters to show some basic relations between parameters with the intension to simplify and stimulate work in coming WIs to define RF core requirements.

In this contribution a text proposal for TR 38.820, subclause 7.2 [1] with additional technical background for how to determine antenna parameters for different array geometries is prepared. The text proposal is attached at the end of the contribution and is presented for approval.

# Discussion

This is a revised version of R4-2006925. The changes are summarized as;

1. The definition of number of elements is clarified, instead of N, now referring to MxNx2.
2. Addition of relevant antenna model symbols in symbol section, subclause 3.2.
3. Clarification on parameter selection when sub-arrays is modelled.
4. Alignment with deployment scenarios used in section 5.
5. In parameter selection procedure text not relevant for the antenna model is removed.
6. Correction of “beam width product” spelling.
7. The technical background for the model was changes according to feedback.
8. Parameters proposed for ITU-R 5D is added as examples.
9. Step 4 and 5 is updated to resolve circular procedure; First select beamwidths based on spacing, then calculate true gain.
10. Table 7.2.4-2 is updated to now include both peak normalized element pattern and peak gain normalized element pattern.
11. Eq. 7.2.4-3 and 7.2.4-4 is updated to consider peak normalized pattern given in Table 7.2.4-2.
12. In step 1, the considered coexistence situation is added.
13. Antenna parameter examples values are removed.
14. A note is introduced in procedure on how to handle sub-arrays.
15. Equation 7.2.4-2 is updated to support the case with symmetrical elements and the case where narrower sub-arrays is used.
16. The reference to IEEE is changes to give more input for the background to 32400 and 52525.

# Conclusion

In this contribution we have summarized the array antenna model and described how antenna model parameters can be determined. Also, some example parameters sets have been created to map towards different antenna topologies.

A text proposal has been created to TR 38.820 [1] with some additional technical background information about the antenna topologies relation to the array antenna model parameters. At the end on this contribution a text proposal for TR 38.820, subclause 7.2 is attached for approval.

# References

[1] R4-2005740, “draft TR 38.820 v130”, Huawei

[2] M.2101, “RecommendationITU-RM.2101-0; Modelling and simulation of IMT networks and systems for use in sharing and compatibility studies”, ITU-R

[3] TR 37.840, “Study of Radio Frequency (RF) and Electromagnetic Compatibility (EMC) requirements for Active Antenna Array System (AAS) base station”, 3GPP

[4] W. L. Stutzman, "Estimating directivity and gain of antennas," in IEEE Antennas and Propagation Magazine, vol. 40, no. 4, pp. 7-11, Aug. 1998, doi: 10.1109/74.730532, URL: <http://ieeexplore.ieee.org/stamp/stamp.jsp?tp=&arnumber=730532&isnumber=15753>

TEXT PROPOSAL for clause 2

# 2 References

The following documents contain provisions which, through reference in this text, constitute provisions of the present document.

- References are either specific (identified by date of publication, edition number, version number, etc.) or non‑specific.

- For a specific reference, subsequent revisions do not apply.

- For a non-specific reference, the latest version applies. In the case of a reference to a 3GPP document (including a GSM document), a non-specific reference implicitly refers to the latest version of that document *in the same Release as the present document*.

[65] W. L. Stutzman, "Estimating directivity and gain of antennas," in IEEE Antennas and Propagation Magazine, vol. 40, no. 4, pp. 7-11, Aug. 1998, doi: 10.1109/74.730532, URL: <http://ieeexplore.ieee.org/stamp/stamp.jsp?tp=&arnumber=730532&isnumber=15753>

TEXT PROPOSAL for clause 3.2

## 3.2 Symbols

For the purposes of the present document, the following symbols apply:

BWChannel BS channel bandwidth

BWSSB Bandwidth of the SSB

COff Isolation in OFF state

Fmax Measure of the achievable power gain

Ft Cut-off frequency

IMF Industrial Margin

Psat Saturated output power

RON Losses in ON state

xFR Integer representing the BS frequency range

AA Composite antenna array pattern in dB

AE Array element pattern in dB

Am Front-to-back ratio in dB

SLAv Side-lobe suppression in dB

3dB Vertical half power beam width in degrees

3dB Horizontal half power beam width in degrees

GE,max Element peak gain in dB

LE Element loss in dB

dh Horizontal element separation

dv Vertical element separation

 Horizontal angle (defined between -180° and 180°).

 Vertical angle of the signal direction (defined between -0° and 180°, 90° represents the direction perpendicular to the antenna array)

TEXT PROPOSAL for subclause 7.2:

### 7.2.3 Antenna topologies

The AA consists of MxNx2 antenna elements placed is a certain lattice. The signals from the AA is mapped in the RDN creating different antenna topologies as shown in figure 7.2.3-1. The RDN mapping is creating sub-arrays, where the radiating characteristics of a sub-array is different to single antenna elements (AE).



Figure 7.2.3-1: Example RDN mappings

### Depending on intended coverage scenarios different types of RDN mappings are foreseen for the frequency range 7 to 24 GHz. For *BS type 1-H* and *BS type 1-O* and *BS type 2-O*, the OTA RF characteristics defined for requirement set category set H and requirement set category O is declared by the base station manufacturer in terms of full array capability as well as sub array or element capability, see TS 38.141-2 [6], clause 4.6.7.2.4 Array Antenna model

In Table 7.2.4-1, the parameters used by the parameterized array antenna model are described. Based on AAS base station architecture and intended deployment scenario, different parameter sets are required to model an AAS base station.

**Table 7.2.4-1: Parameters**

| **Parameter** | **Symbol** | **Unit** |
| --- | --- | --- |
| Front to back ratio | *Am* | dB |
| Side lobe suppression | *SLAv* | dB |
| Horizontal HPBW | *3dB* | Degrees |
| Vertical HPBW | *3dB* | Degrees |
| Element peak gain | *GE,max* | dBi |
| Element loss | *LE* | dB |
| Number of columns and rows | *(M, N)* | Integer |
| Horizontal element separation | *dh* | m |
| Vertical element separation | *dv* | m |
| Electrical down-tilt angle | *etilt* | Degrees |
| Electrical scan angle | *escan* | Degrees |

The parameterized antenna model is built around array antenna model where the element factor, array factor and linear phase progressing is characterized as described by equations in Table 7.2.4-2.

**Table 7.2.4-2: Array antenna model**

| **Description** | **Equation** | **Unit** |
| --- | --- | --- |
| Peak normalized element radiation pattern |  | dB |
| Peak gain normalized element radiation pattern |  | dBi |
| Element peak gain | , where the peak directivity *DE,max*is calculated from given values on *3dB, 3dB, dh* and*dv* | dBi |
| Composite array radiation pattern | , where | dBi |

To conserve complexity the model is created so that the element is gain normalized, instead of the composite array pattern. As a consequence, parameters cannot be selected arbitrary, since parameters are dependent on each other. The intension with the model is to model absolute gain patterns correctly without full pattern directivity normalization. To model absolute gain, parameters must be selected carefully, if not the model produces nonphysical and incorrect gain response.

When array antenna parameters are selected for the array antenna model it is preferable to consider physical aspects such as the gain/area relation and gain/beamwidth relations by checking following aspects in given order;

1. The considered deployment scenario and coexistence situation will give the appropriate coverage range for the horizontal domain and vertical domain.
2. From the coverage ranges and deployment scenario the required antenna gain can be determined, from which the array antenna geometry can be determined in terms of number of vertical rows (*M*), the number of horizontal columns (*N*).
3. From the coverage ranges the array antenna steering capability can be determined in terms element separations (*dv*, *dh*).  
     
   Note: The element separations *dv* and *dh* is the distance between elements in the array antenna. The RDN can be used to create sub-arrays to optimize coverage. When sub-arrays are modelled, parameters can be selected to model the sub-array as a radiating element.
4. From the given array lattice the element parameters can be considered with respect to the given area for a single element. The element peak gain (*GE,max*) and half power beamwidth product (*3dB3dB*) are depend on each other and must be selected together to maintain accurate model gain response. Also, the element loss factor (*LE*) needs to be included when the element peak gain is determined. Select parameter values for beamwidth based on following two parameters checks;
   1. Check the peak element directivity (*DE,max*) with the unit area available for a single element in the array lattice, as described in Eq. 7.2.4-1.
   2. Check the peak element directivity (*DE,max*) with the half-power beam width product (*3dB3dB*), as described in Eq. 7.2.4-2.
5. The model gain is guaranteed by a element peak directivity normalization directivity (*DE,max*) described in Eq. 7.2.4-3. The peak element gain is calculated based on Eq. 7.2.4-4.

From antenna theory the peak element directivity assuming no losses for a given antenna aperture area can be expressed as:

(Eq. 7.2.4-1)

Also, the peak element directivity for a given wide symmetrical beam can be approximated by:

(Eq. 7.2.4-2)

, where *K* is a factor that depends on the element properties. For single elements with symmetrical large beamwidths, *K=52525* is appropriate, while for sub-arrays with narrower beamwidth characteristics, *K=32400* is more appropriate. Depending on the element characteristics the relation between element peak gain and the half power beam width product is different as described in [65].

To be exact it is recommended to select element parameters, where the peak element gain is determined by calculating the directivity from a given geometry including beam widths. The element directivity can be calculated based on the pattern described by Table 7.2.4-1 in dBi as:

(Eq. 7.2.4-3)

, where *A(,)* is defined in linear scale as:

(Eq. 7.2.4-4)