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| 3GPP TR 38.808 V0.0.3 (2020-11) |
| Technical Report |
| 3rd Generation Partnership Project;Technical Specification Group Radio Access Network;Study on supporting NR from 52.6 GHz to 71 GHz(Release 17) |
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Contents

Foreword 5

Introduction 6

1 Scope 7

2 References 7

3 Definitions of terms, symbols and abbreviations 8

3.1 Terms 8

3.2 Symbols 8

3.3 Abbreviations 8

4 Study of Required Changes to NR 8

4.1 RAN1 Aspects 8

4.1.1 Candidate numerology and bandwidth 8

4.2 RAN4 aspects 9

5 Study of channel access mechanism for 60GHz 9

5.1 Identification of regulatory aspects for consideration 9

Annex <A> (informative): Evaluation Methodology 10

A.1 Link level evaluation assumptions 10

A.2 System level evaluation assumptions 10

A.2.1 [Evaluation A] 10

A.2.1 [Evaluation B] 10

Annex <B> (informative): Change history 11

# Foreword

This Technical Report has been produced by the 3rd Generation Partnership Project (3GPP).

The contents of the present document are subject to continuing work within the TSG and may change following formal TSG approval. Should the TSG modify the contents of the present document, it will be re-released by the TSG with an identifying change of release date and an increase in version number as follows:

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x the first digit:

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In the present document, modal verbs have the following meanings:

**shall** indicates a mandatory requirement to do something

**shall not** indicates an interdiction (prohibition) to do something

The constructions "shall" and "shall not" are confined to the context of normative provisions, and do not appear in Technical Reports.

The constructions "must" and "must not" are not used as substitutes for "shall" and "shall not". Their use is avoided insofar as possible, and they are not used in a normative context except in a direct citation from an external, referenced, non-3GPP document, or so as to maintain continuity of style when extending or modifying the provisions of such a referenced document.

**should** indicates a recommendation to do something

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The construction "may not" is ambiguous and is not used in normative elements. The unambiguous constructions "might not" or "shall not" are used instead, depending upon the meaning intended.

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The constructions "can" and "cannot" are not substitutes for "may" and "need not".

**will** indicates that something is certain or expected to happen as a result of action taken by an agency the behaviour of which is outside the scope of the present document

**will not** indicates that something is certain or expected not to happen as a result of action taken by an agency the behaviour of which is outside the scope of the present document

**might** indicates a likelihood that something will happen as a result of action taken by some agency the behaviour of which is outside the scope of the present document

**might not** indicates a likelihood that something will not happen as a result of action taken by some agency the behaviour of which is outside the scope of the present document

In addition:

**is** (or any other verb in the indicative mood) indicates a statement of fact

**is not** (or any other negative verb in the indicative mood) indicates a statement of fact

The constructions "is" and "is not" do not indicate requirements.

# Introduction

This clause is optional. If it exists, it shall be the second unnumbered clause.

# 1 Scope

In order to support wide range of services, 5G NR system aims to be flexible enough to meet the connectivity requirements of a range of existing and future (yet unknown) services to be deployable in an efficient manner. NR considers supporting potential use of frequency range up to 100 GHz [1].

NR specifications that have been developed in Rel-15 and Rel-16 define operation for frequencies up to 52.6 GHz, where all physical layer channels, signals, procedures, and protocols are designed to be optimized for uses under 52.6 GHz.

However, frequencies above 52.6 GHz are faced with more difficult challenges, such as higher phase noise, larger propagation loss due to high atmospheric absorption, lower power amplifier efficiency, and strong power spectral density regulatory requirements in unlicensed bands, compared to lower frequency bands. Additionally, the frequency ranges above 52.6 GHz potentially contain larger spectrum allocations and larger bandwidths that are not available for bands lower than 52.6 GHz.

As an initial effort to enable and optimize 3GPP NR system for operation in above 52.6 GHz, 3GPP RAN has studied requirements for NR beyond 52.6GHz up to 114.25GHz including global spectrum availability and regulatory requirements (including channelization and licensing regimes), potential use cases and deployment scenarios, and NR system design requirements and considerations on top of regulatory requirements [2]. The potential use cases identified in the study include high data rate eMBB, mobile data offloading, short range high-data rate D2D communications, broadband distribution networks, integrated access backhaul (IAB), factory automation, industrial IoT (IIoT), wireless display transfer, augmented reality (AR)/virtual reality (VR) wearables, intelligent transport systems (ITS) and V2X, data center inter-rack connectivity, smart grid automation, private networks, and support of high positioning accuracy. The use cases span over several deployment scenarios identified in the study. The deployment scenarios include, but not limited to, indoor hotspot, dense urban, urban micro, urban macro, rural, factor hall, and indoor D2D scenarios. The study also identified several system design requirements around waveform, MIMO operation, device power consumption, channelization, bandwidth, range, availability, connectivity, spectrum regime considerations, and others.

Among the frequencies of interest, frequencies between 52.6 GHz and 71 GHz are especially interesting relatively in the short term because of their proximity to sub-52.6 GHz for which the current NR system is optimized and the imminent commercial opportunities for high data rate communications, e.g., unlicensed spectrum but also licensed spectrum between 57 GHz and 71 GHz. Therefore, it would be beneficial to make a study focused on feasibility of using existing waveforms and required changes for frequencies between 52.6 GHz and 71 GHz, so as to take advantage of imminent commercial opportunities for the specific frequency regime by minimizing the specification burden and maximizing the leverage of FR2 based implementations.

# 2 References

The following documents contain provisions which, through reference in this text, constitute provisions of the present document.

- References are either specific (identified by date of publication, edition number, version number, etc.) or non‑specific.

- For a specific reference, subsequent revisions do not apply.

- For a non-specific reference, the latest version applies. In the case of a reference to a 3GPP document (including a GSM document), a non-specific reference implicitly refers to the latest version of that document *in the same Release as the present document*.

[1] 3GPP TR 38.913: "Study on Scenarios and Requirements for Next Generation Access Technologies"

[2] 3GPP TR 38.807: "Study on requirements for NR beyond 52.6 GHz".

[3] 3GPP TR 21.905: "Vocabulary for 3GPP Specifications".

 [4] ETSI EN 302 567 v2.1.20: "Multiple-Gigabit/s radio equipment operating in the 60 GHz band; Harmonised Standard covering the essential requirements of article 3.2 of Directive 2014/53/EU".

[5] R1-2007549 "Further discussion on B52 numerology" FUTUREWEI.

[6] R1-2007558 "Discussion on physical layer impacts for NR beyond 52.6 GHz" Lenovo, Motorola Mobility.

[7] R1-2007604 "PHY design in 52.6-71 GHz using NR waveform" Huawei, HiSilicon.

[8] R1-2007642 "Physical layer design for NR 52.6-71GHz" Beijing Xiaomi Software Tech.

[9] R1-2007652 "Discussion on required changes to NR using existing DL/UL NR waveform" vivo.

[10] R1-2007785 "Consideration on required changes to NR using existing NR waveform" Fujitsu.

[11] R1-2007790 "Consideration on supporting above 52.6GHz in NR" InterDigital, Inc.

[12] R1-2007847 "System Analysis of NR opration in 52.6 to 71 GHz" CATT.

[13] R1-2007883 "Required changes to NR using existing DL/UL NR waveform" TCL Communication Ltd.

[14] R1-2007926 "Required changes to NR using existing DL/UL NR waveform" Nokia, Nokia Shanghai Bell.

[15] R1-2007929 "On phase noise compensation for NR from 52.6GHz to 71GHz" Mitsubishi Electric RCE.

[16] R1-2009379 "Discussion on Required Changes to NR in 52.6 – 71 GHz" Intel Corporation.

[17] R1-2007965 "On the required changes to NR for above 52.6GHz" ZTE, Sanechips.

[18] R1-2007982 "On NR operations in 52.6 to 71 GHz" Ericsson.

[19] R1-2008045 "Consideration on required physical layer changes to support NR above 52.6 GH" LG Electronics.

[20] R1-2008076 "Discussion on required changes to NR using existing DL/UL NR waveform in 52.6GHz ~ 71GHz" CMCC.

[21] R1-2008082 "Study on the numerology to support 52.6 GHz to 71GHz" NEC.

[22] R1-2008872 "Design aspects for extending NR to up to 71 GHz" Samsung.

[23] R1-2008250 "Discusson on required changes to NR using DL/UL NR waveform" OPPO.

[24] R1-2008353 "Considerations on required changes to NR from 52.6 GHz to 71 GHz" Sony.

[25] R1-2008457 "A Discussion on Physical Layer Design for NR above 52.6GHz" Apple.

[26] R1-2008493 "Discussions on required changes on supporting NR from 52.6GHz to 71 GHz" CAICT.

[27] R1-2008501 "On required changes to NR using existing DL/UL NR waveform for operation in 60GHz band" MediaTek Inc.

[28] R1-2008516 "On NR operation between 52.6 GHz and 71 GHz" Convida Wireless.

[29] R1-2009062 "Evaluation Methodology and Required Changes on NR from 52.6 to 71 GHz" NTT DOCOMO, INC.

[30] R1-2008615 "NR using existing DL-UL NR waveform to support operation between 52p6 GHz and 71 GHz" Qualcomm Incorporated.

[31] R1-2008726 "Discussion on physical layer aspects for NR beyond 52.6GHz" WILUS Inc.

[32] R1-2008769 "Waveform considerations for NR above 52.6 GHz" Charter Communications.

[33] R1-2007550 "On channel access modes in 60GHz" FUTUREWEI.

[34] R1-2007559 "Discussion on channel access for NR beyond 52.6 GHz" Lenovo, Motorola Mobility.

[35] R1-2008976 "Channel access mechanism for 60 GHz unlicensed operation" Huawei, HiSilicon.

[36] R1-2007643 "Channel access mechanism for NR on 52.6-71 GHz" Beijing Xiaomi Software Tech.

[37] R1-2007653 "Discussion on channel access mechanism" vivo.

[38] R1-2007791 "On Channel access mechanisms" InterDigital, Inc.

[39] R1-2007848 "Channel Access Mechanism in support of NR operation in 52.6 to 71 GHz" CATT.

[40] R1-2007884 "Channel access mechanism" TCL Communication Ltd.

[41] R1-2007918 "Channel access mechanisms for NR from 52.6-71GHz" AT&T.

[42] R1-2007927 "Design of NR channel access mechanisms for 60 GHz unlicensed band" Nokia, Nokia Shanghai Bell.

[43] R1-2009380 "Channel Access Procedure for NR in 52.6 - 71 GHz" Intel Corporation.

[44] R1-2007966 "On the channel access mechanism for above 52.6GHz" ZTE, Sanechips.

[45] R1-2007983 "Channel Access Mechanism" Ericsson.

[46] R1-2008046 "Considerations on channel access mechanism to support NR above 52.6 GHz" LG Electronics.

[47] R1-2008091 "Discussion on channel access mechanism for above 52.6GHz" Spreadtrum Communications.

[48] R1-2008157 "Channel access mechanism for 60 GHz unlicensed spectrum" Samsung.

[49] R1-2008251 "Discussion on channel access" OPPO.

[50] R1-2008354 "Channel access mechanism for 60 GHz unlicensed spectrum" Sony.

[51] R1-2008458 "Views on Channel Access Mechanisms for Unlicensed Access above 52.6 GHz" Apple.

[52] R1-2008494 "Discussions on channel access mechanism on supporting NR from 52.6GHz to 71 GHz" CAICT.

[53] R1-2008517 "On Channel Access Mechanism and Interference Handling for Supporting NR from 52.6 GHz to 71 GHz" Convida Wireless.

[54] R1-2008548 "Channel Access Mechanism for NR in 60 GHz unlicensed spectrum" NTT DOCOMO, INC.

[55] R1-2008563 "Discussion on channel access mechanism" ITRI.

[56] R1-2009362 "Channel access mechanism for NR in 52p6 to 71GHz band" Qualcomm Incorporated.

[57] R1-2008717 "Discussion on channel access mechanism for 52.6 to 71GHz unlicensed ban" Potevio

[58] R1-2008770 "Further aspects of channel access mechanisms" Charter Communications.

[59] R1-2007560 "Additional evaluations for NR beyond 52.6GHz" Lenovo, Motorola Mobility.

[60] R1-2007654 "Evaluation on different numerologies for NR using existing DL/UL NR waveform" vivo.

[61] R1-2007792 "Evaluation results for above 52.6 GHz" InterDigital, Inc.

[62] R1-2007928 "Simulation Results for NR from 52.6 GHz to 71 GHz" Nokia, Nokia Shanghai Bell.

[63] R1-2007943 "Considerations on performance evaluation for NR in 52.6-71GHz" Intel Corporation.

[64] R1-2007967 "Simulation results for NR above 52.6GHz" ZTE, Sanechips.

[65] R1-2007984 "Evaluation results for NR in 52.6 - 71 GHz" Ericsson.

[66] R1-2008047 "Considerations on phase noise compensation to support NR above 52.6 GHz" LG Electronics.

[67] R1-2008873 "Evaluation results for extending NR to up to 71 GHz" Samsung.

[68] R1-2009615 "Discussion on other aspects" OPPO.

[69] R1-2008459 "Evaluation results for Physical Layer Design for NR above 52.6GHz" Apple.

[70] R1-2009062 "Potential Enhancements for NR on 52.6 to 71 GHz" NTT DOCOMO, INC.

[71] R1-2008771 "Performance evaluations for NR above 52.6 GHz" Charter Communications.

[72] R1-2009610 "Link level and System level evaluation for NR system operating in 52.6GHz to 71GHz" Huawei, HiSilicon.

# 3 Definitions of terms, symbols and abbreviations

## 3.1 Terms

For the purposes of the present document, the terms given in 3GPP TR 21.905 [3] and the following apply. A term defined in the present document takes precedence over the definition of the same term, if any, in 3GPP TR 21.905 [3].

## 3.2 Symbols

For the purposes of the present document, the following symbols apply:

B transmission bandwidth

G antenna gain

## 3.3 Abbreviations

For the purposes of the present document, the abbreviations given in 3GPP TR 21.905 [3] and the following apply. An abbreviation defined in the present document takes precedence over the definition of the same abbreviation, if any, in 3GPP TR 21.905 [3].

BS Base Station

EIRP Equivalent Isotropic Radiated Power

FDD Frequency Duplex Division

IAB Integrated Access Backhaul

ISM Industrial, Scientific and Medical

ITU International Telecommunication Union

LBT Listen Before Talk

MCOT Maximum Channel Occupancy Time

NR New Radio

OCB Occupied Bandwidth

OOBE Out-Of-Band Emission

PSD Power Spectral Density

PTP Point to point

SCS Subcarrier spacing

SI Study Item

SID Study Item Description

TDD Time Duplex Division

UE User Equipment

V2X Vehicle to Everything

WAN Wide Area Network

# 4 Study of required changes to NR

## 4.1 RAN1 Aspects

### 4.1.1 General description of study in RAN1

For supporting NR operation in both licensed and unlicensed band in the frequency range from 52.6 GHz to 71 GHz, FR2 numerologies and additional numerologies beyond that supported currently in NR are studied. Existing framework for numerology scaling is considered i.e. 2μ ×15 subcarrier spacing to select the candidates. For SSB transmissions, it is investigated whether or not µ > 4 (larger than 240 kHz) is needed and corresponding impacts, if any, on the aspects including at least SSB pattern, multiplexing of other signal/channels, and transmission window, if supported. For data and control channel transmissions, it is investigated if µ > 3 (larger than 120 kHz) is needed and corresponding impacts, if any, on aspects including at least processing timelines, PDCCH monitoring capability (BD/CCE), scheduling enhancements, beam-management, and reference signal design. For investigating the need for higher numerologies, some of the key aspects that are studied are the impact due to phase noise, delay spread, TAE, analog beam switching delay, and impact to coverage, spectral efficiency and peak data rates, and relative delay in intra-cell/inter-cell multi-TRP operations.

### 4.1.2 Candidate numerology and bandwidth

*Editor’s Note: This section can include discussion on CP length, subcarrier spacing, and channel bandwidth issues*

### 4.1.3 Investigation of physical layer impact from candidate numerology and bandwidths

*Editor’s Note: This section can include discussion on potential specification impact that stem from introduction of candidate numerology and bandwidths*

## 4.2 RAN4 aspects

*Editor’s Note: This section will be further categorized into sub-sections depending on discussions*

# 5 Study of channel access mechanism for 60 GHz

*Editor’s Note: This section will be further categorized into sub-sections depending on discussions*

## 5.1 Identification of regulatory aspects for consideration

*Editor’s Note: This section can include list of identified regulatory aspects that is needed for consideration of channel access mechanism for 60 GHz unlicensed operation.*

## 5.2 Channel access and interference mitigation techniques

*Editor’s Note: This section can include study of channel access and interference mitigation techniques.*

# 6 Summary of evaluation study

## 6.1 Summary of link level evaluations

7 sources, [65], [30], [60], [68], [25], [29], and [16], reported evaluation results of PSS/SSS detection performance in terms of SINR in dB achieving cell ID detection probability of 90% by one-shot detection from PSS/SSS. 4 sources, [65], [30], [60], and [25], reported PBCH performance in terms of SINR in dB achieving PBCH BLER target of 10%. 2 sources, [9], and [65], compared link budget of SSB for difference SCS.

- For PSS and SSS detection performance, all evaluated candidate SCSs (120, 240, 480 and 960 kHz) show comparable performances with the channel models and delay spread values parameters provided in Table A.1-1. The following were observed from the evaluations:

- The performance degrades as the increase of SCS

- 6 out of 7 sources reported minor performance difference (< or ~ 1 dB) between adjacent SCS for all evaluated candidate SCSs (120, 240, 480 and 960 kHz). The other source [25] reported more than 3 dB performance gap of 960 kHz SCS compared to other 120, 240 and 480 kHz SCS. It also reported that the gap of 960 kHz increases as the delay spread increases.

- For PBCH BLER performance, all evaluated candidate SCSs (120, 240, 480 and 960 kHz) show comparable performances with the channel models and delay spread parameters provided in Table A.1-1.

- The performance degrades as the increase of SCS.

- All 4 sources reported minor performance difference (< or ~ 1 dB) between adjacent SCS for all evaluated candidate SCSs (120, 240, 480 and 960 kHz).

- The performance gap between 120 and 960 kHz is up to ~ 1.8 dB.

- In terms of SSB link budget, smaller SCS have better coverage than larger SCS.

- The MCL and MIL difference between 120 kHz SCS and 480 kHz SCS is about 5 dB. The MCL and MIL difference between 120 kHz SCS and 960 kHz SCS is about 8 dB.

8 sources, [65], [72], [30], [60], [64], [68], [29], and [16], reported evaluation results of PRACH preamble detection performance in terms of SINR in dB achieving PRACH preamble misdetection probability of 1% with evaluation assumptions and parameters as in Table A.1-1. Two sources, [65], and [20], compared link budget of PRACH for different SCS. The following are observed:

- For PRACH preamble detection performances for the same PRACH format, all evaluated candidate SCSs (120, 240, 480 and 960 kHz) show comparable performances.

- 7 out of 8 sources reported minor performance difference (< or ~ 1 dB) between adjacent SCS for all evaluated candidate SCSs (120, 240, 480 and 960 kHz). The other source [68] reported minor performances difference among all SCS for TDL-A with 5 and 10ns delay spread. It reported infinite SINR for 960 kHz SCS and comparable SINR for 120, 240 and 480 kHz SCS in TDL-A with 20ns delay spread using the metrics of preamble miss detection probability of 1% and the estimated timing error is within [-Tcp/2, Tcp/2].

- For PRACH link budget of the same PRACH format and the same sequence length, maximum isotropic loss (MIL) and maximum coupling loss (MCL) degrade as the subcarrier spacing is increased, negatively impacting coverage.

- Two sources, [65], and [23], reported that with UE power limitation of 25 dBm EIRP, the MCL/MIL difference between 120 kHz SCS and 480 kHz SCS is about 4 to 5 dB; the MCL/MIL difference between 120 kHz SCS and 960 kHz SCS is about 8 dB.

- One source [65] reported that without UE power limitation of 25 dBm EIRP (but still under regulatory limits), the MCL difference between 120 kHz SCS and 480 kHz SCS is less than 2.5 dB; the MCL difference between 120 kHz SCS and 960 kHz SCS is less than 1 dB.

- One source [65] reported that without UE power limitation of 25 dBm EIRPs (but still under regulatory limits), compared to short PRACH sequence length, longer PRACH sequence length improve MCL/MIL significantly for 120 kHz SCS due to wider bandwidth for a given SCS.

For CP-OFDM, the following are observed regarding the impact of DMRS to BLER performance.

- One source [61] reported performance improvement with increased number of DMRS symbols or increased DMRS density especially for higher modulation order for 960 kHz SCS in TDL-A (5 ns and 10 ns delay spread).

- One source [18] reported for 480 kHz SCS and below with large delay spread (TDL-A with 40 ns delay spread), the room for performance improvement with a change to the Rel-15 DMRS design is very limited.

- One source [16] reported a performance drop when frequency domain OCC is enabled especially for higher order modulation such as 64 QAM (MCS 22) for 960 kHz SCS in TDL-A (10ns and 20 ns delay spread) and 480 kHz SCS (20 ns delay spread). The performance gap increases when channel delay spread increases.

- One source [30] reported performance improvement with a new DMRS pattern featured by high frequency density (i.e., every RE) and 2-FD-OCC across adjacent REs for 960 kHz SCS in TDL-A (20 ns and 40 ns delay spread).

- One source [14] reported that with Rel-15 DMRS type-1, different delay spread values (10ns and 20ns) have a negligible impact to the demodulation performance of PDSCH for a high SCS (such as 960 kHz).

7 sources, [65], [72], [30], [60], [68], [14], and [25], evaluated DFT-S-OFDM PUSCH BLER performance with different SCS.

- Compared to CP-OFDM when CPE-only compensation is enabled, DFT-s-OFDM is more robust under phase noise.

- For low and medium MCSs (QPSK and 16QAM), there’s minor performance difference among evaluated SCSs up to 960 kHz.

- With normal CP, for high MCS (64QAM), the performance improves as the increase of SCS, 120 kHz SCS shows up to ~2.0dB loss compared to other larger SCS.

- One source [65] reported a performance gap of 1.4 ~ 1.8 dB between 120 and 960 kHz SCS.

- One source [72] reported a performance gap of 1.3 ~ 2.5 dB between 120 and 960 kHz SCS.

- One source [30] reported a performance gap of 1.2 ~ 1.7 dB between 120 and 960 kHz SCS.

- One source [60] reported a performance gap of ~ 1.4 dB between 120 and 960 kHz SCS.

- One source [14] did not report numerical SINR results in table but provided figures showing approximately similar performance difference, ~ 2 dB, between 120 and 960 kHz SCS.

- One source [25] reported a performance gap of more than 7 dB performance gap between 120 kHz SCS and other SCS (240, 480 and 960 kHz) at TDL-A 5 ns DS. It also reported 120 kHz SCS cannot meet the BLER target of 10% at TDL-A 10ns DS and 960 kHz SCS cannot meet the BLER target of 10% at TDL-A 20ns DS.

- Another source [68] reported 120 and 240 kHz SCS cannot meet the BLER target of 10% for all evaluated DS values.

- For high MCS (64QAM) at large delay spread (TDL-A 40ns or CDL-B 50ns DS), there’s error floor for 960 kHz SCS at least for BLER target 1%.

- One source [30] reported an error floor for 960 kHz SCS for BLER target 1%.

- One source [60] reported an error floor for 960 kHz SCS for BLER target 10%.

- One source [68] reported no error floor of 960 kHz SCS for the BLER target of 10% and 1% for CDL-B 50ns but an error floor for 960 kHz SCS at TDL-A 20ns for BLER target 1%.

For CP-OFDM, with evaluation assumptions and parameters as in Table A.1-1, the following are observed when CPE-only compensation based on the existing Rel-15 NR PTRS structure is used for normal CP when delay spread is not large. The performance is measured in terms of SINR in dB achieving BLER target of 10% or 1%.

- For low MCS (QPSK) and medium MCS (16QAM), there is minor performance difference between different SCS values up to 960 kHz.

- For high MCS (64QAM), the performance improves in general as the increase of SCS.

- For high MCS (64QAM), 13 sources, [65], [72], [30], [60], [64], [68], [14], [6], [59], [25], [22], [29], [16], and [11], compared performance of 120 and 240 kHz SCS in 400 MHz bandwidth.

o For 10% BLER target, there is a performance gap between 120kHz and 240kHz SCS where 240 kHz SCS performs better.

- One source [65] reported better performance of 240 kHz SCS in CDL-D. It also reported both SCS cannot meet 10% BLER target for other evaluated channel model.

- 3 sources, [72], [68], and [14], reported both SCS cannot meet 10% BLER target.

- 4 sources, [60], [64], [25], and [11], reported 120 kHz SCS cannot meet 10% BLER target, while 240 kHz SCS can.

- One source, [6] and additional results in [59], reported better performance of 240 kHz SCS at TDL-A 5 and 10ns. It also reported that both SCS cannot meet 10% BLER target for other evaluated cases.

- One source [16] reported better performance of 240 kHz SCS in CDL-D. It also reported that both SCS cannot meet 10% BLER target for other evaluated cases.

- 2 sources, [30], and [22], reported better performance of 240 kHz SCS.

- One source [29], reported comparable performance for both SCS in CDL-D. It also reported better performance of 120 kHz SCS for the other evaluated channel models.

- For high MCS (64QAM), 13 sources, [65], [30], [60], [64], [68], [14], [6], [59], [25], [22], [29], [16], [71], and [11], compared performance of 240 and 480 kHz SCS in 400 MHz bandwidth.

- for 10% BLER target, there is a performance gap between 240kHz and 480kHz SCS where 480 kHz SCS performs better.

- One source [65] reported better performance for 480 kHz SCS in CDL-D. It also reported 240 kHz SCS cannot meet 10% BLER target for other evaluated channel model.

- 3 sources, [68], [14], and [71], reported 240 kHz SCS cannot meet 10% BLER target, while 480 kHz SCS can.

- One source [6] and additional results in [59], reported better performance of 480 kHz SCS at TDL-A 5 and 10ns. It also reported 240 kHz SCS cannot meet 10% BLER target for other evaluated cases.

- One source [16] reported better performance of 480 kHz SCS in CDL-D. It also reported 240 kHz SCS cannot meet 10% BLER target for other evaluated cases.

- 6 sources, [30], [60], [64], [25], [22], and [11], reported better performance of 480 kHz SCS.

- One source [29], reported comparable performance for both SCS in CDL-D. It also reported better performance of 240 kHz SCS for the other evaluated channel models.

- For high MCS (64QAM), 14 sources, [65], ,[72], [30], [60], [64], [68], [14], [6], [59], [25], [22], [29], [16], [71], and [11], compared performance of 480 and 960 kHz SCS in 400 MHz bandwidth.

- For 10% BLER target, there is a performance gap between 480kHz and 960kHz SCS where 960 kHz SCS performs better.

- 7 sources, [65], [64], [68], [14], [6], [59], [71], and [11], reported a greater than 1 dB gain of 960 kHz SCS.

- 3 sources, [30], [60], and [22], reported a smaller than 1 dB performance gain of 960 kHz SCS.

- One source [72] reported better performance of 480 kHz SCS for CDL-B 50ns and better performance of 960 kHz SCS for other evaluated cases. In all comparison, the difference is greater than 1 dB.

- Two sources, [25], and [16], reported a better performance of 480 kHz SCS than 960 kHz SCS at 20ns DS in TDL-A where 960 kHz SCS cannot meet 10% BLER target and comparable performance for both SCS in all other evaluated cases.

- One source [29] reported comparable performance for both SCS in CDL-D. It also reported better performance of 480 kHz SCS in TDL-A 5ns and better performance of 960 kHz SCS in CDL-B 20ns.

- For 1% BLER target, the performance for 960kHz SCS is better than 480kHz SCS.

- Among sources reported SINR values when both SCS can meet 1% BLER target, the absolute value of the performance gap between 480 kHz and 960 kHz SCS is larger than that for 10% BLER target.

- For high MCS (64QAM), 4 sources, [65], [60], [14], and [22], compared performance of 480 and 960 kHz SCS in 1600 or 2000 MHz bandwidth. 4 out of 4 sources reported performance gain around 4 ~ 5 dB of 960 kHz SCS for 10% BLER target. All 4 sources also reported that 480 kHz SCS cannot meet 1% BLER target.

For CP-OFDM, with evaluation assumptions and parameters as in Table A.1-1 (including optional delay spread value), the following are observed when CPE-only compensation based on the existing Rel-15 NR PTRS structure is used with respect to CP type and large delay spread.

- When delay spread is not large (< 40 ns in TDL-A), there is minor performance difference between normal and extended CP for SCS values up to 960 kHz when compared on the basis of equal MCS (code rate). If comparing on the basis of equal TBS (equal throughput), the performance of ECP is degraded due to higher overhead of ECP.

- Among 11 sources, [65], [72], [30], [60], [64], [68], [6], [59], [5], [29], [16], and [11], evaluated with large delay spread (i.e. 40 ns in TDL-A and/or 50ns in CDL) based on the existing Rel-15 NR PTRS structure for normal CP, 10 sources observed that for low MCS (QPSK) and medium MCS (16QAM), there is minor performance difference between different SCS values up to 960kHz for 10% BLER target.

- The other source [5] evaluated SCS 960 kHz with CPE compensation at MCS16 with normal CP in TDL-A channel with 40ns DS. It reported that the BLER for SCS 960 kHz, MCS16, and Normal CP is not acceptable (cannot meet 10% BLER target) for 40ns DS.

- 10 sources, [65], [72], [30], [60], [64], [68], [6], [59], [29], [16], and [11], evaluated large delay spread (i.e. 40 ns in TDL-A and/or 50ns in CDL) with CPE compensation based on the existing Rel-15 NR PTRS structure with normal CP. Among 10 sources, 5 sources, [18], [72], [9], [60], [6], [59], and [29], also evaluated extended CP at least for 960 kHz SCS with CPE compensation based on the existing Rel-15 NR PTRS structure.

- 9 out 10 sources observed that for high MCS (64QAM) with normal CP, larger SCS (480 and 960 kHz) performs better than smaller SCS (120 and 240 kHz) when only CPE compensation based on the existing Rel-15 NR PTRS structure is used. The other source [29] reported better performance of smaller SCS.

- 5 out 5 sources observed the performance of 960 kHz SCS with extended CP is significantly improved compared to with normal CP for large delay spread case when compared on the basis of equal MCS (code rate).

- 4 sources, [18], [72], [9], [6], and [59], compared throughput of normal CP and extended CP at least for 960 kHz SCS with CPE compensation based on the existing Rel-15 NR PTRS structure. They all reported worse throughput of extended CP.

For CP-OFDM, the following are observed with respect to phase noise compensation and PTRS.

- Compared to no phase noise compensation, CPE compensation shows little gain at low and medium MCSs for all the evaluated SCS values; while significant gain is observed for high MCS (64QAM) for all the evaluated SCS values.

- Two sources, [61], and [15], reported that increased PTRS density in frequency domain based on Rel-15 configuration does not provide significant performance benefits.

- For a given SCS, the complexity of ICI compensation increases as the number of ICI filter tap increases

- For MCS 22 evaluation of the same SCS, performance gain of ICI compensation with additional complexity of multi-tap filtering compared to CPE-only compensation is observed when there is sufficient number of PTRS in the frequency domain for 120, 240 and 480 kHz SCS.

- One source [65] showed performance gain of ICI compensation compared to CPE-only compensation for all evaluated SCS

- One source [72] evaluated ICI compensation and compared with CPE-only compensation. It reported performance gain for all evaluated SCS.

- One source [30] compared the performance of CPE and ICI compensation for 120 kHz SCS reported performance gain of ICI compensation.

- One source [68] compared the performance of CPE and ICI compensation for all SCS. It reported performance gain of ICI compensation for 240 kHz and 480 kHz SCS. It reported performance gain of ICI compensation in CDL-B but a performance loss in TDL-A for 960 kHz SCS. It also reported that 120 kHz SCS still cannot meet 10% BLER target with ICI compensation.

- One source [14] reported performance gain of ICI compensation for 120, 240 and 480 kHz SCS. It also reported performance gain of ICI compensation for 960 kHz SCS at 2GHz bandwidth and a performance loss of ICI compensation for 960 kHz SCS at 400MHz bandwidth.

- One source [69] evaluated ICI compensation for different SCS with a new PTRS pattern. It reported improvement of ICI compensation compared to CPE-only compensation.

- One source [22] evaluated 120 kHz and 240 kHz SCS performance with ICI compensation based on some new PTRS pattern and reported performance improvement.

- One source [5] compared ICI performance among SCS. It reported performance gain of multi-tap ICI filter over CPE compensation for 120, 240 and 480 kHz SCS.

- One source [16] evaluated performance of de-ICI method for MCS 22 with small RB allocations for 240, 480 and 960 kHz SCS. It is observed that the de-ICI method do not work when there isn’t sufficient number of PTRS tones in the frequency domain.

- For MCS 22 with normal CP when delay spread is not large, it is observed that ICI compensation of multi-tap filtering is required for 120, 240 and/or 480 kHz SCS to achieve comparable performance (< 1 dB difference) to that of 960 kHz SCS with CPE-only compensation for 10% BLER target

- 2 sources, [65], and [14], reported comparable performance of 480 kHz SCS with ICI compensation and 960 kHz SCS with CPE compensation in 1600 MHz bandwidth

- 2 sources, [68], and [14], reported comparable performance of 480 kHz SCS with ICI compensation and 960 kHz SCS with CPE compensation in 400 MHz bandwidth

- One source [72] reported comparable performance of 240 kHz SCS with ICI compensation and 960 kHz SCS with CPE compensation in 400 MHz bandwidth

- One source [30] evaluated and compared 120 kHz SCS with ICI compensation to larger SCS with CPE compensation. It reported that at MCSs 22 and 24, 120 kHz SCS with ICI compensation performs almost equal to 960 kHz SCS with CPE-only compensation in 400 MHz bandwidth.

- One source [5] reported comparable performance of 480 kHz SCS with ICI compensation and 960 kHz SCS with CPE compensation in TDL-A 5 and 10ns as well as in CDL-D 30ns in 400 MHz bandwidth.

- At very high MCS (e.g., MCS 26 or MCS 28), three sources, [16], [30], and [73], compared ICI and CPE compensation using the Rel-15 PTRS.

- One source [16] evaluated the phase noise compensation performance with MCS 28 when delay spread is not large. It is observed that de-ICI technique with 3-taps filter for smaller subcarrier spacing (240 kHz) fails even though there are sufficient number of PTRS tones available for ICI covariance construction.

- One source [30], compared the performance of CPE and ICI compensation and reported for MCS 26, 120kHz SCS with ICI compensation suffers from residual ICI and is outperformed by 960kHz SCS with CPE-only compensation when delay spread is not large.

- One source [72] showed that for MCS 28, de-ICI technique with large number of taps (11, 9 and 7 taps for 120, 240 and 480 kHz SCS respectively) outperforms 960 kHz with CPE compensation only when delay spread is not large. For normal CP, it also reported that 960 kHz with 3-tap ICI compensation has comparable performance to other SCS with larger number of taps (11, 9 and 7 taps for 120, 240 and 480 kHz SCS respectively) for MCS 28 when delay spread is not large. It also reported that with large delay spread (50ns in CDL), ECP and ICI compensation with at least 3 taps filter are needed for 960 kHz SCS to reach 1% BLER target for MCS 26.

- For high MCS (64QAM) with normal CP when delay spread is large (TDL-A with 40 ns and/or CDL-B with 50ns), 4 sources compared performance of smaller SCS (120, 240 and/or 480 kHz) with ICI compensation to that of 960 kHz SCS with CPE compensation and reported worse performance of 960 kHz SCS with CPE compensation for 10% BLER target.

- One source [65] reported a performance gain of 5 dB in TDL-A 40ns and 0.3 dB in CDL-B 50ns for 480 kHz SCS with ICI compensation compared to 960 kHz SCS with CPE compensation in 1600 MHz bandwidth.

- One source [72] reported a performance gain of 2.6 dB (for 240 kHz SCS) and 1.6 dB (for 120 kHz SCS) in CDL-B 50ns with ICI compensation compared to 960 kHz SCS with CPE compensation.

- One source [68] reported a performance gain of 1 dB in CDL-B 50ns for 480 kHz SCS with ICI compensation compared to 960 kHz SCS with CPE compensation. It also reported the performance of 120 kHz with ICI compensation cannot meet the 10% BLER target.

- One source [5] reported the performance of 960 kHz SCS with CPE compensation cannot meet the 10% BLER target. It also reported that the performance of 480 kHz SCS with ICI compensation cannot meet the 10% BLER target in TDL-A 40ns. With ICI compensation, it also reported comparable performance of 120, 240 and 480 kHz SCS in CDL-B 50ns and comparable performance of 120 and 240 kHz SCS in TDL-A 40ns.

- Multiple sources evaluated and compared ICI compensation schemes using the existing Rel-15 NR distributed PTRS structure and/or new PTRS patterns. The results from different sources are not aligned on whether new PTRS patterns perform better than existing Rel-15 PTRS structure when ICI compensation is used.

- One source [15] evaluated with 120 and 240 kHz SCS and reported that the PN compensation with block-based PTRS and cyclic sequence significantly outperforms in spectral efficiency both CPE compensation and de-ICI Wiener filtering with distributed PTRS, even when the density of the scattered pattern is increased above the Rel.15 defined density.

- One source [18] reported that 3-tap direct de-ICI compensation with Rel-15 PTRS outperforms ICI filter approximation approach with clustered PTRS. 3-tap direct de-ICI compensation with a clustered PTRS structure does not offer any performance advantage over the existing Rel-15 NR distributed PTRS structure.

- One source [27] reported that with a 3-tap BLS ICI equalizer, a clustered PTRS structure does not offer any performance advantage over the existing Rel-15 NR distributed PTRS structure.

- One source [66] reported that the performance of clustered PTRS allocation is worse than that of Rel-15 PTRS based ICI compensation scheme and further showed that the performance of subcarrier nulling allocation is similar or superior (up to 2 dB gain especially in the scenarios with low PTRS overhead, K=4) to that of Rel-15 PTRS based ICI compensation scheme.

- Two sources, [22], and [69], evaluated the performance with some new PTRS patterns (e.g. chunk based PTRS pattern to allow adjacent PTRS symbols in frequency) and reported that the performance with ICI compensation based on new PTRS patterns is better than the Rel-15 pattern with CPE compensation only.

- One source [30] reported that for the same ICI compensation algorithm, the legacy PTRS pattern outperforms the block PTRS pattern. It showed that for ICI compensation (direct de-ICI filtering) with the legacy PTRS pattern, the performance improves with the increasing number of de-ICI filter taps (3 to 5 taps). It also observed that with a fixed transport block size, the performance improves as the PTRS overhead decreases (the performance loss due to increased effective code rate is more pronounced at higher MCSs) and with a fixed effective code rate, the performance slightly improves as the PTRS overhead increases.

- For high MCS (64QAM) with normal CP, 2 sources, [65], and [14], compared performance of 480 and 960 kHz SCS in 1600 MHz bandwidth when ICI compensation is used based on Rel-15 PTRS.

- When delay spread is not large, both sources reported a smaller than 1 dB performance gain of 960 kHz SCS for both 10% and 1% BLER target in TDL-A. One source, [65], reported that for CDL-B, there is up to 1.1 dB gain at 1% BLER target for 960 kHz SCS.

- When delay spread is large (TDL-A with 40 ns DS), one source, [65], reported 480 kHz SCS performed 3.6 dB better than 960 kHz SCS at 10% BLER target and 960 kHz SCS cannot meet the 1% BLER target.

For CP-OFDM, two sources, [65], and [72], evaluated PDSCH BLER performance with optional PN models in addition to PN model in Table A.1-1. Note that such optional PN models are not confirmed and/or recommended by RAN4 at the time of RAN1#103-e.

- When CPE-only compensation is used with an optional PN model at the UE or at BS and UE, it is observed by both sources that there is significantly less dependence of BLER performance on SCS compared to the PN model in Table A.1-1. For all test cases, no error floor is observed for smaller SCS with TDL-A or CDL-B/CDL-D for 1% BLER target. There is around 1 to 2 dB performance difference between consecutive SCSs for 1% BLER target.

- However, multiple sources expressed concerns on the validity of such optional PN models given no confirmation and/or recommendation from RAN4. In consequence, there’s a concern on whether and how the observations based on such optional PN models can be used given no RAN4 input on these optional PN models.

## 6.2 Summary of system level evaluations

For comparison of No-LBT (NLBT) and Tx side ED based omnidirectional sensing (TxED-Omni) for Indoor scenario A, 6 Companies have compared No-LBT with Tx Side ED based Omni sensing TxED-Omni LBT and provide following observations:

- Source [37], show tail and median benefits of using TxED-Omni LBT on DL, at high loading. In other cases, including all loads for UL and other loads for DL, TxED-Omni LBT scheme shows losses. All results are at ED threshold -47 dBm.

- Source [16] shows gains for 5%ile DL throughput at high loads with TxED-Omni LBT. In other cases including all loads for UL and other loads for DL, TxED-Omni LBT scheme shows losses. All results are at ED threshold -47 dBm.

- Source [65], [35], [42], [56] and [67] show loss for TxED-Omni LBT with an EDT of -47 dBm or -48 dBm for all cases.

# Annex A: Evaluation methodology

## A.1 Link level evaluation assumptions

This subclause describes the link level simulation assumptions used for evaluations. The link level simulation assumption is given in Tables A.1-1. The primary objective of the evaluation is to evaluate performance of PDSCH/PUSCH including study of phase noise impairment impact for various numerology (i.e. subcarrier spacing, CP length) and possibly for various carrier frequencies. The evaluation KPI(s) include BLER. The secondary objective of the evaluation is to evaluate performance of SSB/PRACH including study of phase noise impairment impact for various numerology (i.e. subcarrier spacing, CP length) and possibly for various carrier frequencies. Evaluation KPI(s) include miss-detection, and false alarm.

Table A.1-1: Link level evaluation assumptions and parameters

| Assumptions | Value |
| --- | --- |
| Carrier Frequency [GHz] | 60 GHz Optional: 70 GHz |
| Subcarrier Spacing [kHz] | PDSCH/PUSCH:- {120, 240, 480, 960} kHz-optional: 1920 kHzOptional:- if evaluated companies are asked to provide information on other channels/signals and subcarrier spacing |
| Bandwidth [MHz] | PDSCH/PUSCH:- {400, 2000} MHz Optional:- Companies are asked to provide information if other bandwidths are evaluatedNote: Evaluation of listed channel bandwidth does not mean RAN1 has agreed to support such channel bandwidth and are only for evaluation purposes to obtain useful insights. |
| Number of RB | For 400 MHz:- 256 (120 kHz),- 128 (240 kHz),- 64 (480 kHz),- 32 (960 kHz),- N/A (1920 kHz)For 2000 MHz:- N/A (120 kHz),- N/A (240 kHz),- 320 (480 kHz) (optional),- 160 (960 kHz),- 80 (1920 kHz), For other channel bandwidths:- Companies are asked to provide information. Companies are encouraged to utilize linearly scaled PRB sizes for a given bandwidth based on above.Note: Other bandwidth and sub-carrier spacing combinations can be optionally used. |
| Waveform | For PDSCH:CP-OFDMFor PUSCH:CP-OFDM and DFT-s-OFDM |
| CP Type | Normal CPExtended CPNote: ECP is not expected to be applicable in all SCS and channel conditions, and companies providing results for ECP are encouraged to provide evaluation results with motivation/justification of simulated ECP cases |
| Channel Model | TDL model as defined in of TR38.901 Section 7.7.2:- TDL-A (5ns, 10ns, 20ns DS) - optional DS for consideration: 40ns, 60ns DS CDL model as defined in of TR38.901 Section 7.7.1:- CDL-B (20ns, 50ns DS)- CDL-D (20ns, 30ns DS) with K-factor = 10 dB- optional DS for consideration: 100ns DS Optional modification CDL-B/D model(a) Indoor Office NLOS: CDL-B (20 ns DS), and Indoor Office LOS: CDL-D (20 ns DS)- Use mean angular spread values from Table 7.5.6-Part2 (for ASD, ASA, and ZSA) and Table 7.5-10 (for ZSD)- Use mean angles of CDL-B/D for desired mean angles as baseline (no angle translation)- Note that the angular spread values in the table are quoted in log units- Mean K-factor for CDL-D from Table 7.5.6-Part2 (9 dB)(b) UMi – Street Canyon NLOS: CDL-B (50 ns DS), and UMi – Street Canyon LOS: CDL-D (30 ns)- Use mean angular spread values from Table 7.5.6-Part1 (for ASD, ASA, and ZSA) and Table 7.5-8 (for ZSD).- Use mean angles of CDL-B/D for desired mean angles as baseline (no angle translation)- Note that the angular spread values in the table are quoted in log units- Use mean K-factor for CDL-D from Table 7.5.6-Part1 (7 dB)Note: Mean angular spread values are used as desired AS value to scale the ray angles as described in TR38.901 section 7.7.5.1. As baseline, the ray angles are not translated, meaning (TR38.901 section 7.7.5.1). If companies perform translation of the ray angles they are encouraged to report the details. The mean K-factor is used to scale the tap powers as described in TR38.901 section 7.7.6.Note 2: for TDL/CDL model, the delay spread (DS) value mentioned is the delay spread scaling value (i.e. corresponding to normalized delay of 1.0).Note 3: Other models (either TDL or CDL) with DS values not listed are optional. Note 4: Companies are encouraged to provide evaluation results with motivation/justification of simulated DS values. |
| Antenna Configuration (Mg,Ng,M,N,P) | For TDL model:- 2x2- 1x2 (optional)For CDL model:Configuration 1:- (Mg,Ng,M,N,P) = (1,1,8,16,2) BS with (0.5 dv, 0.5 dH)- (Mg,Ng,M,N,P) = (1,1,4,4,2) UE with (0.5 dv, 0.5 dH)Configuration 2:- (Mg,Ng,M,N,P) = (1,1,4,8,2) BS with (0.5 dv, 0.5 dH)- (Mg,Ng,M,N,P) = (1,1,2,2,2) UE with (0.5 dv, 0.5 dH) |
| Mobility | 3 km/hr |
| PA Model | Optional:- Companies to provide modelling (in lieu of pre-loaded Tx EVM) |
| gNB TRP PN Model | 3GPP TR38.803 example 2 BS PN profileOptional:- If other PN profile is used, companies to provide information on the modelling usedNote: companies to provide information about the LO distribution model assumed in the simulations. |
| UE PN Model | 3GPP TR38.803 example 2 UE PN profileOptional:- If other PN profile is used, companies to provide information on the modelling usedNote: companies to provide information about the LO distribution model assumed in the simulations. |
| Pre-loaded Tx EVM | Optional:- 3% at Tx (In lieu of PA model),- If other values are used companies are asked to provide information on the values selected for simulation. |
| Additive Rx EVM | Optional:- 5% at Rx,- If other values are used companies are asked to provide information on the values selected for simulation. |
| I-Q Imbalance | Optional:- (-26dBc),- (-31dBc),- If other values are used companies are asked to provide information on the values selected for simulation. |
| Frequency Offset | Optional:- 0.1 ppm (for PDSCH/PUSCH)- 5, 10, 20 ppm (for initial access) |
| Channel Estimation | Realistic channel estimation |
| Transmission Rank | Rank 1Note: companies are asked to provide information the precoding scheme (including granularity) used in the evaluations. |
| PDSCH SLIV | (S=2, L=12)Optional:(S=0, L=14)Note: Starting symbol, S, (indexed from 0) and length, L. |
| DMRS Configuration | 1 DMRS symbol (front loaded), or 2 DMRS symbols at (2,11) symbol indexNote: no data multiplexing is assumed in DMRS symbols |
| PTRS Configuration | For CP-OFDM:(K = 4, L = 1) or (K = 2, L = 1)Note: PTRS per K number of PRBs, and PTRS every L number of OFDM symbolsFor DFT-s-OFDM:(Ng = 2, Ns = 2, L = 1)(Ng = 2, Ns = 4, L = 1)(Ng = 4, Ns = 2, L = 1)(Ng = 4, Ns = 4, L = 1)(Ng = 8, Ns = 4, L = 1)Note: Ng number of PT-RS groups, Ns number of samples per PT-RS group, and PTRS every L number of DFT-s-OFDM symbolsNote 2: companies are asked to provide the PT-RS configuration used for DFT-s-OFDM simulation among the listed above, where the selection of the PT-RS is chosen such that it provides similar overhead as the chosen PT-RS configuration for PUSCH CP-OFDM (if simulated). |
| CSI-RS / TRS | CSI-RS/TRS is assumed to be off (for RS overhead) |
| MCS/TBS | From MCS Table 1 (TS38.214):- MCS 7 (QPSK),- MCS 16 (16QAM),- MCS 22 (64QAM),From MCS Table 2 (TS38.214):- MCS 27 (256QAM) (optional)Assume NohPRB = 0 for MCS calcuations.Note: If normal CP and extended CP are to be compared, companies are asked to provide information on the MCS values used that provide similar payload sizes for the comparison. Companies to provide actual code rate used in the evaluations. |

## A.2 System level evaluation assumptions

This subclause describes the system level simulation assumptions used for evaluations. The system level simulation assumption is given in Tables A.2-1. The primary objective is evaluation of single operator and multi-operator deployments including study of interference impact and coexistence between nodes. The evaluation KPI(s) include user throughput, latency, average buffer occupancy, ratio of mean served throughput and offered cell throughput, and resource utilization. The secondary objective is to obtain delay spread profiles (and inter-symbol interference statistics) for deployment scenarios of interest. Note that performance impact from delay spread should be conducted in link level simulations, the system level simulations would be used to supplement the findings.

Table A.2-1: System level evaluation assumptions and parameters

| Assumptions | Value |
| --- | --- |
| Carrier Frequency [GHz] | 60 GHzOptional: 70 GHz |
| Subcarrier Spacing [kHz] | For 2000MHz BW:- 960 kHz- optional: 120, 240, 480 kHzFor 400MHz BW:- 120 kHz- optional: 240, 480, 960 kHzNote: Other than value above, companies are encouraged to evaluating using subcarrier spacing values determined to be feasible from LLS study. Values for the subcarrier spacing may be revisited after further investigation from LLS study. |
| Bandwidth [MHz] | 2000 MHz400 MHz Note: Channel bandwidth evaluated may be revisited after further investigation. |
| Number of RB | For 2000 MHz:- N/A (120 kHz),- N/A (240 kHz),- 320 (480 kHz) (optional),- 160 (960 kHz),- 80 (1920 kHz),For 400 MHz:- 256 (120 kHz),- 128 (240 kHz),- 64 (480 kHz),- 32 (960 kHz),- N/A (1920 kHz) For other channel bandwidths:- Companies are asked to provide information. Companies are encouraged to utilize linearly scaled PRB sizes for a given bandwidth based on above. |
| Deployment Scenario | - Scenario indoor-A (for two operator case)- Scenario indoor-C (for single operator case)**Secondary scenarios:**- Scenario outdoor-BOptional:- other scenarios listed below**Indoor Office:****Scenario Indoor-A)** InH open office model:Office box 120m x 50 m, 12 BS per operator, 2 operator, BS height at 3m (ceiling), UE height 1m, x-axis ISD = 20m and y-axis ISD = 25m, where ISD is define by the distance between two adjacent 10m x 10m virtual box, BS randomly deployed within 10m x 10m virtual box, minimum distance between BS of different operators is 2m.Optional: single operator deployment in Scenario Indoor-A **Scenario Indoor-B)** small InH open office model:Office box 20m x 20 m, 1 BS per operator, 2 operator, BS height at 3m (ceiling), UE height 1m, BS randomly deployed within 10m x 10m virtual box, minimum distance between BS of different operators is 2m. **Scenario Indoor-C)** InH open office model:Office box 120m x 50 m, 12 BS per operator, 1 operator, BS height at 3m (ceiling), UE height 1m, BS fixed position, ISD = 20m **Scenario Indoor-D)** InH open office model:Office box 120m x 50 m, 6 BS per operator, 2 operator, BS height at 3m (ceiling), UE height 1m, BS fixed position, ISD = 20mFFS: if the office box scenario can be reduced down to 50m x 50m **Scenario Indoor-E)** InH open office model:Office box 120m x 80 m, 3 BS per operator, 2 operator, BS height at 3m (ceiling), UE height 1m, BS fixed position, a=20m, b=40m, c=20m, and d=40mimage001 **Dense Urban:****Scenario Outdoor-A)** Dense Urban with 1 layerHexagonal grid, single layer, 3 sectors per site, 7 sites locations, BS height 10m, UE height 1.5m, ISD = 150mFFS: whether ISD needs to be smalleroptional: Reducing deployment size from 7 sites to 1 site with wrap around **Scenario Outdoor-B)** Dense Urban with 2 layersMacro layer (sub 7GHz – not necessarily need to be simulated for the 60GHz evaluation): Hexagonal grid, single layer, 3 sectors per site, 7 sites locationsBS height 25m, UE height 1.5m, ISD = 100m, fixed BS positionMicro layer (above 52.6 GHz):BS height 10m, UE height 1.5m, 2 operator, 2 BS per hexgrid per operator, random position within macro hexagonal grid per operator, minimum distance between TRP and UE: 10m, minimum distance between micro gNBs’ of the same operator: 10moptional: Reducing deployment size from 7 sites to 1 site with wrap around. **Scenario Outdoor-C)** Dense Urban with 1 layerHexagonal grid, single layer, 3 sectors per site, 3 sites locations, BS height 10m, UE height 1.5m, ISD = 150m **Indoor Factory Hall:****Scenario Factory-A)** Indoor factory with Dense cluster & low BS (InF-DL)Grid, 300m x 150m x 10m factor hallISD 50m, BS height 1.5m, UE height 1.5m, Typical clutter size 2m, Clutter height 6m, Clutter density 60%**Scenario Factory-B)** Indoor factory with sparse clutter & High BS (InF-SH)Grid, 300m x 150m x 10m factor hallISD 50m, BS height 8m, UE height 1.5m, Typical clutter size 10m, Clutter height 2m, Clutter density 20% |
| UE distribution | Average of 5 or 10 UE per BS UE are either 100% indoor or 100% outdoor depending on deployment scenario. |
| Channel Model | **InH open office:**- gNB-to-gNB and gNB-to-UE links: InH – office channel & PL model from TR38.901, indoor – open office LOS probability from TR38.901 (optional: indoor – mixed office LOS probability from TR38.901)- UE-to-UE links: InH – office channel & PL model from TR38.901, indoor – mixed office LOS probability from TR38.901 **Dense Urban:**- gNB-to-gNB and gNB-to-UE links: UMi street canyon channel & PL model from TR38.901- UE-to-UE links: [outdoor to outdoor D2D channel & PL model from TR36.843 Section A.2.1.2], [(optional: UMi street canyon channel & PL model from TR38.901)] **Indoor factory:**- gNB-to-gNB and gNB-to-UE links: InF channel & PL model from TR38.901- UE-to-UE links: [InF channel & PL model from TR38.901]Note: 3D distance between an gNB and a UE is applied. 3D distance is also used for LOS probability and break point distance.Note: channel models in brackets, [ ], are working assumption and may be revisited.Note: For D2D channel model used for UE-to-UE links companies should report how they scaled the model to 60 GHz. |
| Mobility | 3 km/hr |
| BS Antenna Configuration (Mg,Ng,M,N,P) | For outdoor macro/sectorized scenarios:(Mg,Ng,M,N,P) = (1,1,8,16,2)with (0.5 dv, 0.5 dH)For outdoor micro-layer scenarios:(Mg,Ng,M,N,P) = (1,3,8,16,2)with (0.5 dv, 0.5 dH)Note: 3 Panel single sector gNB with {0,+120,-120} degree boresight orientations. The gNB will only utilize 1 panel at given moment.For indoor scenarios:(Mg,Ng,M,N,P) = (1,1,4,8,2) with (0.5 dv, 0.5 dH)optional: (Mg,Ng,M,N,P) = (1,1,8,16,2) per pol with (0.5 dv, 0.5 dH) |
| BS Antenna Pattern | For outdoor scenarios:- Antenna power pattern given in Table 7.3-1 of TR38.901(with exception of antenna element gain)For indoor scenarios:- Antenna power pattern given in Table A.2.1-7 of TR38.802 for ceiling mount(with exception of antenna element gain)For factory scenarios:Companies to provide information on the antenna orientation and pattern used. |
| BS Antenna element gain | 5 dBi |
| UE Antenna Configuration (Mg,Ng,M,N,P) | Configuration 1: (Mg,Ng,M,N,P) = (1,2,2,2,2)with (0.5 dv, 0.5 dH)Configuration 2 (optional):(Mg,Ng,M,N,P) = (1,2,4,4,2)with (0.5 dv, 0.5 dH)Note: In both configurations, the 2 panels are back-to-back with panel selection done the at receiver. The UE will only utilize 1 panel at a given moment. |
| UE Antenna Pattern | Antenna power pattern given in Table A.2.1-8 of TR38.802For indoor factory scenarios:Boresight orientation should be fixed in all simulation dropsFor other scenarios:Boresight orientation should be randomized between [0°, 360°) in the horizontal plane in each simulation dropNote: Companies to provide information about boresight orientation (e.g. random orientation, vertical to ground, parallel to ground, etc) |
| UE Antenna element gain | 5 dBi |
| BS Power Limitation | 40 dBm EIRP Optional: 60 dBm EIRPMaximum TxP adjusted to meet EIRP limits |
| UE Power Limitation | 25 dBm EIRP with 21 dBm max TxP Optional: 40dBm EIRP with 21 dBm max TxP |
| BS NF | 7 dB |
| UE NF | 10 dBOptional: 13dB |
| Transmission Rank | Rank adaptative transmission between Rank 1 and 2 |
| PDCCH Overhead | 2 symbol per slot |
| DMRS Overhead | 1 symbol per slot |
| CSI-RS Overhead | Companies to provide information |
| SRS Overhead | Companies to provide information |
| Other Overhead | Companies to provide information |
| Data Processing Latency | UE processing timeline in microseconds are assumed to be same as 120 kHz SCS PDSCH/PUSCH processing latencyOptional:UE processing timeline in microseconds are assumed to be half of 120 kHz SCS PDSCH/PUSCH processing latency |
| TDD DL/UL Ratio | Companies to provide information (if applicable) |
| CSI feedback | Ideal feedback |
| Additive Rx EVM | Note: additive Rx EVM values may be revisited after LLS study |
| Traffic Model | FTP Model 3 (27Mbyte file) Optional: - Full buffer,- FTP Model 1 (27, 8 Mbyte file),- FTP Model 3 (0.5, 2, 8, 16 Mbyte file) |
| UE Receiver | MMSE-IRC |
| Cell selection criteria | Random select from strongest RSRP with 1 dB HO MarginNote: UE with RSRP below a -71 dBm + 10 log10( bandwidth/2GHz ) are not considered in simulation and not counted toward UE distribution count |
| DL/UL Traffic Ratio | 50% DL, 50% UL Optional:100% DL, 0% UL,80% DL, 20% UL0% DL, 100% UL |
| Channel access modelling | Companies to report details of LBT procedure and parameters (e.g. ED, CWmax, COT, etc.) if LBT procedure is used in the evaluations. |
| Synchronization Assumption | Companies are asked to provide information on the synchronization assumption made between operators for 2 operator deployment scenarios. |

## A.3 LBT procedure for system level evaluation

This subclause describes the LBT procedure assumed for system level simulation evaluations. Figure A.3-1 shows an illustration of the LBT procedure assumed for system level simulation evaluations. LBT procedures in draft v2.1.20 of EN 302 567 as the baseline system evaluation with LBT [4]. When the node is performing CCA before initiating transmission, during count down, when an observation slot fails energy detect (ED), the counter freezes, and will continue count down 8 μs after the interference is detected to be gone. Any enhancements to ED threshold, contention window sizes, Zmin and Zmax, can be considered as part of the evaluations. The smallest value of Zmax for contention window size is 3, and Zmin is equal to 0.



Figure A.3-1: Illustration of LBT procedure assumed for system level simulation evaluations

# Annex B: Evaluations results

## B.1 Link level evaluation results

*Editor’s Note: This section will be potentially sub-divided into further sub-sections depending on case and/or scenario.*

### B.1.1 Evaluation results for PDSCH/PUSCH

*Editor’s Note: template for the evaluation results is presented as a placeholder for now.*

Table B.1.1-1: LLS template: SINR in dB achieving PDSCH/PUSCH BLER of 10% /1%

|  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- |
| Tdoc /Source | MCS | Channel | 120KHz/400MHz | 240KHz/400MHz | 480KHz/400MHz | 960KHz/400MHz | 960KHz/2GHz |
| R1-xxxxxxx / Source 1 | 7 | TDL-A, 5ns | X / Y (X for 10% BLER, Y for 1% BLER) |  |  |  |  |
| TDL-A, 10ns |  |  |  |  |  |
| TDL-A, 20ns |  |  |  |  |  |
| CDL-B, 20ns |  |  |  |  |  |
| CDL-B, 50ns |  |  |  |  |  |
| CDL-D, 20ns |  |  |  |  |  |
| CDL-D, 30ns |  |  |  |  |  |
| 16 | TDL-A, 5ns |  |  |  |  |  |
| TDL-A, 10ns |  |  |  |  |  |
| TDL-A, 20ns |  |  |  |  |  |
| CDL-B, 20ns |  |  |  |  |  |
| CDL-B, 50ns |  |  |  |  |  |
| CDL-D, 20ns |  |  |  |  |  |
| CDL-D, 30ns |  |  |  |  |  |
| 22 | TDL-A, 5ns |  |  |  |  |  |
| TDL-A, 10ns |  |  |  |  |  |
| TDL-A, 20ns |  |  |  |  |  |
| CDL-B, 20ns |  |  |  |  |  |
| CDL-B, 50ns |  |  |  |  |  |
| CDL-B, 20ns |  |  |  |  |  |
| CDL-B, 50ns |  |  |  |  |  |
| Additional report/notes:1. CP type
2. antenna configuration for CDL model
3. waveform in case of PUSCH
4. PTRS configuration
5. DMRS configuration
6. any optional or other assumption/parameters used not as in the baseline
 |

### B.1.2 Evaluation results for PSS/SSS

*Editor’s Note: template for the evaluation results is presented as a placeholder for now.*

Table B.1.2: LLS template: SINR in dB achieving cell ID detection probability of 90% by one-shot detection from PSS/SSS

|  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- |
| Tdoc /Source | Channel | 120KHz | 240KHz | 480KHz | 960KHz |
| R1-xxxxxxx / Source 1 | TDL-A, 5ns |  |  |  |  |
| TDL-A, 10ns |  |  |  |  |
| TDL-A, 20ns |  |  |  |  |
| CDL-B, 20ns |  |  |  |  |
| CDL-B, 50ns |  |  |  |  |
| CDL-D, 20ns |  |  |  |  |
| CDL-D, 30ns |  |  |  |  |
| Additional report/notes: 1. frequency offset
2. the number and granularity of the frequency locations
3. antenna configuration for CDL model
4. any optional or other assumption/parameters used not as in the baseline
5. false alarm rate
6. criteria for PSS detection success
 |

### B.1.3 Evaluation results for PRACH

*Editor’s Note: template for the evaluation results is presented as a placeholder for now.*

Table B.1.3-1: LLS template: SINR in dB achieving PRACH preamble misdetection probability of 1% and corresponding false alarm probability

|  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- |
| Tdoc /Source | Channel | 120KHz | 240KHz | 480KHz | 960KHz |
| R1-xxxxxxx / Source 1 | TDL-A, 5ns | X / Y (X for SINR in dB to reach 1% misdetection, Y for corresponding false alarm probability in % at that SINR) |  |  |  |
| TDL-A, 10ns |  |  |  |  |
| TDL-A, 20ns |  |  |  |  |
| CDL-B, 20ns |  |  |  |  |
| CDL-B, 50ns |  |  |  |  |
| CDL-D, 20ns |  |  |  |  |
| CDL-D, 30ns |  |  |  |  |
| Additional report/notes: 1. PRACH format2. values of $N\_{cs}$3. antenna configuration for CDL model4. any optional or other assumption/parameters used not as in the baseline |

## B.2 System level evaluation results

*Editor’s Note: This section will be potentially sub-divided into further sub-sections depending on case and/or scenario. Template for the evaluation results is presented as a placeholder for now.*

Table B.2-1: System level evaluation results for scenario

|  |  |  |  |
| --- | --- | --- | --- |
| Tdoc /Source | Cases | Case 1 |  Case 2 |
| R1-xxxxxxx / Source 1 | Traffic loadMetrics  | Low load10%~25% BO  | Medium load35%~50% BO | High loadabove 55% BO | Low load10%~25% BO  | Medium load35%~50% BO | High loadabove 55% BO |
| DL UPT (Mbps) | 5%ile |  |  |  |  |  |  |
| 50%ile |  |  |  |  |  |  |
| 95%ile |  |  |  |  |  |  |
| mean |  |  |  |  |  |  |
| DL delay (s) | 5%ile |  |  |  |  |  |  |
| 50%ile |  |  |  |  |  |  |
| 95%ile |  |  |  |  |  |  |
| mean |  |  |  |  |  |  |
| UL UPT (Mbps) | 5%ile |  |  |  |  |  |  |
| 50%ile |  |  |  |  |  |  |
| 95%ile |  |  |  |  |  |  |
| mean |  |  |  |  |  |  |
| UL delay (s) | 5%ile |  |  |  |  |  |  |
| 50%ile |  |  |  |  |  |  |
| 95%ile |  |  |  |  |  |  |
| mean |  |  |  |  |  |  |
| Arrival rate (files/s) |  |  |  |  |  |  |
| 𝜌DL |  |  |  |  |  |  |
| 𝜌UL |  |  |  |  |  |  |
| BO |  |  |  |  |  |  |
| Additional report/notes:1. LBT procedure and parameters2. any assumptions/parameters used not as in the agreed baseline3. Details of case: e.g., single or two operators; no-LBT, omni-directional LBT, directional LBT schemes etc.4. Other metric(s) and definition if reported5. Details of COT sharing if used in evaluation |

# Annex C: Change history

|  |
| --- |
| **Change history** |
| **Date** | **Meeting** | **TDoc** | **CR** | **Rev** | **Cat** | **Subject/Comment** | **New version** |
| 2020-10 |  | R1- R1-2007958 |  |  |  | Draft skeleton TR  | V0.0.2 |
| 2020-11 |  | R1-200xxxx |  |  |  | Updated TR based on agreements from RAN1 #103-e. | V0.0.3 |
| 2020-11 | RAN#90e | RP-20xxxx |  |  |  |  | V1.0.0 |