TSG-RAN Working Group 4 (Radio) meeting #113R4-2420385

Orlando, Florida, USA, 18th to 22nd November 2024

**Title: LS Reply on Parameters for 14800 to 15350 MHz of terrestrial component of IMT for sharing and compatibility studies in preparation for WRC-27**

**Response to: LS R4-2400333 on Parameters of terrestrial component of IMT for sharing and compatibility studies in the frequency bands 4 400-4 800 MHz, 7 125-8 400 MHz and 14.8-15.35 GHz**

**Release: Rel-19**

**Work Item: FS\_NR\_IMT\_4400\_7125\_14800MHz**

**Source: TSG RAN WG4**

**To: ITU-R WP 5D**

**Cc: RAN**

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**Send any reply LS to: 3GPP Liaisons Coordinator,** mailto:3GPPLiaison@etsi.org

**Attachments:** -

1 Overall description

RAN WG4 received the incoming LS from ITU-R Working Party 5D on Parameters of terrestrial component of IMT for sharing and compatibility studies in preparation for WRC-27 ([Att. 7.4 to 5D/134](https://www.itu.int/dms_ties/itu-r/md/19/wp5d/c/R19-WP5D-C-0134%21H07%21MSW-E.docx)) and would like to thank for the opportunity to give input on this topic.

RAN WG4 has already replied for the 4400-4800 MHz frequency range ([R4-2410576](https://www.3gpp.org/ftp/tsg_ran/WG4_Radio/TSGR4_111/Docs/R4-2410576.zip)) and for the 7125-8400 MHz frequency range ([R4-2414449).](https://www.3gpp.org/ftp/tsg_ran/WG4_Radio/TSGR4_112/Docs/R4-2414449.zip) The recommended IMT technology related parameters for the frequency range 14800 to 15350 MHz are given in Annex 1 of this LS. The following should be noted:

* AAS limits always apply Over-the-Air (OTA).
* AAS BS type (i.e. Hybrid AAS vs. OTA AAS requirements set; FR1 vs. FR2 frequency assignment) for 14800 to 15350 MHz frequency range is not specified.
* Non-AAS BS architecture section has been removed as not applicable for 14800 to 15350 MHz frequency range.

RAN4 is developing a technical report (TR 38.922) on the IMT parameters described in this LS, which will be published end of 2024.

The recommended IMT antenna characteristics are given in Annex 2 of this LS. The following should be noted:

* Parameters are interdependent and derived as a package, based on deployment scenarios and other requirements.
* An omni directional UE antenna with 0dBi gain and no beamforming, was agreed as the worst-case for co-existence simulation purposes. Therefore, UEs are not included in the table. More information on other possible UE architecture are described in [3].

RAN4 would also like to provide the following additional information related to AAS implementations for the frequency bands as described in this LS.

* For MIMO model, M.2101 is sufficient and suitable for pure LOS channel, refer to [3] for the simulation methodologies and results.
* For adjacent channel, refer to [3] for technical background related to additional information

2 Actions

**To ITU-R WP5D**

**ACTION:** 3GPP RAN WG4 asks ITU-R WP 5D to consider the following information provided for 14800 to 15350 MHz in Annex 1 and Annex 2, as well as the information related to AAS implementations for the frequency bands in the abovementioned LS from ITU-R Working Party 5D.

3 Dates of next TSG RAN WG 4 meetings

TSG-RAN4 Meeting #114 Athens, Greece 17-21 February 2025

TSG-RAN4 Meeting #114bis TBC, China 07-11 April 2025

TSG-RAN4 Meeting #115 St. Julians, Malta 19-23 May 2025

ANNEX 1

**IMT technology-related and deployment-related parameters for bands between 14800 and 15350 MHz**

**Table 1: IMT technology related parameters in 14800 – 15350 MHz**

|  |  | **IMT**  |
| --- | --- | --- |
| **No.** | **Parameter** | **Base station(AAS)** | **Mobile station** |
| **1** | **Duplex Method** | TDD |
| **2** | **Channel bandwidth (MHz)** | 200 MHz typical (Note 1)  |
| **3** | **Signal bandwidth (MHz)** | Signal bandwidth = NRB × SCS × 12 (Note 2) |
| **4** | **Transmitter characteristics** |  |
| 4.1 | Power dynamic range (dB) | 0 dB | 56 dB typical |
| 4.2 | Spectral mask (dB) | Category A: (Note 3)See table 1A (Wide Area BS) (ΔfOBUE = 100 MHz) | Emission mask for 200 MHz BW is based on the CA mask as defined in [2], § 6.5A.2.2. |
| 4.3 | ACLR  | 31 dB | 24 dB (Note 4) |
| 4.4 | Spurious emissions | Category A: (Note 3)See Table 2A (Wide Area BS)  | Spurious emissions are based on the requirement as defined in [2], § 6.5.3 Table 6.5.3.1-2 with OOB boundary given in Table 6.5A.3.1-1. |
| 4.5 | Maximum output power | See Item No. 1.13 in Table 4 for typical values | 23 dBm typical (Note 2) |
| **5** | **Receiver characteristics** |  |
| 5.1 | Noise figure (dB) | 8 dB (Wide Area BS)13 dB (Medium Range BS)16 dB (Local Area BS)For BS class definitions, see [1], § 4.4 | 13 dB |
| 5.2 | Sensitivity (dBm) | To be specified | To be specified |
| 5.3 | Blocking response  | In-band blocking level: To be specifiedOut-of-band blocking level: See Table 3A for radiated requirements, (ΔfOOB = 100 MHz) | 200 MHz BW requirements the same as [2], § 7.6A Tables 7.6A.2.1-1 and 7.6A.3-1 Bandwidth Class C for blocking levelsand § 7.7 Table 7.7A-1 Bandwidth Class C for spurious response |
| 5.4 | ACS  | 30 dB | 24 dB |
| 5.5 | SINR operating range (dB) | See below “SINR operating range and mapping function”  |

Note 1: Refer to [3] for more information on other values for channel bandwidth and maximum output power.

Note 2: The relevant NRB and SCS for this range is to be defined.

Note 3: Base station Operating band unwanted emissions define all unwanted emissions in the supported downlink operating band plus the frequency ranges extending ΔfOBUE above and ΔfOBUE below each band. Base station Unwanted emissions outside of this frequency range are limited by the spurious emissions requirement.

Note 4: User equipment (UE) ACLR value is derived considering the UE needs to meet the Occupied bandwidth (OBW) requirements, and is higher than the ACLR needed for co-existence.

Note 5: Base Station Out-of-band blocking applies from 30 MHz to 2nd harmonic of the upper frequency edge of the operating band, excluding the in-band blocking frequency range, but including the downlink frequency range in case of an FDD operating band. Requirements are defined assuming a receiver desensitization of 6 dB.

References used in the Table:

[1] [3GPP TS 38.104 v18.7.0, “NR; Base Station (BS) radio transmission and reception”](https://www.3gpp.org/ftp/Specs/archive/38_series/38.104/38104-i70.zip)

[2] [3GPP TS 38.101-1 v18.7.0, “NR; User Equipment (UE) radio transmission and reception; Part 1: Range 1 Standalone”](https://www.3gpp.org/ftp/Specs/archive/38_series/38.101-1/38101-1-i70.zip)

[3] 3GPP TR 38.922, “Study on International Mobile Telecommunications (IMT) parameters for 4400 - 4800 MHz, 7125 - 8400 MHz and 14800 - 15350 MHz”.

TABLE 1A

AAS BS Spectral mask (Operating band unwanted emissions limits) for 14800 - 15350 MHz operation (Category A)

| **Frequency offset of measurement filter ‑3dB point from the carrier frequency, Δf** | **Basic limits** | **Measurement Bandwidth** |
| --- | --- | --- |
| 0 MHz £ Df < 50MHz | $$2dBm-\frac{7}{50}\left(\frac{f\\_offset}{MHz}-0.05\right)$$ | 100 kHz |
| 50 MHz £ Df < min(100 MHz, Dfmax) | -14 dBm | 100 kHz |
| 100 MHz £ Df £ Dfmax | -13 dBm | 1 MHz |
| NOTE: Dfmax is equal to f\_offsetmax minus half of the bandwidth of the measuring filter, where f\_offsetmax is the offset to the frequency ΔfOBUE = 100 MHz outside the downlink operating band. |

TABLE 2A

AAS BS Spurious emissions for 14800 - 15350 MHz operation (Category A)

|  |  |  |  |
| --- | --- | --- | --- |
| Frequency range | Limit | Measurement Bandwidth | Note |
| 30 MHz – 1 GHz | -13 dBm | 100 kHz | Note 1 |
| 1 GHz – 2nd harmonic of the upper frequency edge of the DL operating band | 1 MHz | Note 1, Note 2 |
| NOTE 1: Bandwidth as in ITU-R SM.329, s4.1NOTE 2: Upper frequency as in ITU-R SM.329, s2.5 table 1. |

TABLE 3A

OTA out-of-band blocking performance requirement for 14800 – 15350 MHz operation

| Frequency range of interfering signal(MHz) | Wanted signal mean power(dBm) | Interferer RMS field-strength (V/m) | Type of interfering signal |
| --- | --- | --- | --- |
| 30 to 12750 | EISREFSENS + 6 dB | 0.36  | CW |
| 12750 to FUL,low – 100 | EISREFSENS + 6 dB | 0.1 | CW |
| FUL,high + 100 to 2nd harmonic of the upper frequency edge of the *operating band* | EISREFSENS + 6 dB | 0.1 | CW |

**SINR operating range and mapping function**

The following equations approximate the throughput over a channel with a given SINR, when using link adaptation:

$$Throughput \left(SINR\right) [bps/Hz] =\left\{\begin{array}{c}0 for SINR\leq SINR\_{MIN} \\α∙S\left(SINR\right) for SINR\_{MIN}<SINR<SINR\_{MAX} \\α∙S\left(SINR\_{MAX}\right) for SINR \geq SINR\_{MAX} \end{array}\right.$$

Where:

* $S\left(SINR\right)$: Shannon bound, $S(SINR) =log\_{2}(1+SINR) [bps/Hz]$;
* $α$: Attenuation factor, representing implementation losses;
* $SINR\_{MIN}$: Minimum SINR of the code set [dB];
* $SINR\_{Max}$: Maximum SINR of the code set [dB];
* $The SINR values specified in Table 2 below are in dB but must be converted to linear scale in the formula above.$

The parameters, $SINR\_{MIN}$ and $SINR\_{MAX}$ can be chosen to represent different modem implementations and link conditions. The parameters proposed in Table 2 represent a baseline case, which assumes:

* 1:1 antenna configurations
* AWGN channel model
* Link Adaptation (see Table 2 for details of the highest and lowest rate codes)
* No HARQ

**Table 2: Parameters describing baseline Link Level performance for 5G NR**

|  |  |  |  |
| --- | --- | --- | --- |
| **Parameter**  | **DL**  | **UL**  | **Notes**  |
| $$α$$ | 0.6  | 0.4  | Represents implementation losses  |
| $SINR\_{MIN}$ [dB] | -10  | -10  | Based on QPSK, 1/8 rate (DL) & 1/5 rate (UL)  |
| $SINR\_{Max}$ [dB] | 30  | 22  | Based on 256QAM 0.93(DL) & 64QAM 0.93 (UL)  |

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ANNEX 2

**Antenna characteristics for IMT AAS base stations**

An extended version of the AAS array antenna model is created to support vertical sub-array geometries with fixed sub-array down-tilt. The model equations are summarized in Table 3.

**Table 3: Extended AAS model**

| **Description** | **Equation** |
| --- | --- |
| Peak normalized element radiation pattern | $$A\left(θ,φ\right)=-min\left[-\left(-min\left[12\left(\frac{φ}{φ\_{3dB}}\right)^{2},A\_{m}\right]-min\left[12\left(\frac{θ-90}{θ\_{3dB}}\right)^{2},SLA\_{v}\right] \right),A\_{m}\right]$$ |
| Peak gain normalized element radiation pattern | $$A\_{E}\left(θ,φ\right)=G\_{E,max}+A\left(θ,φ\right)$$ |
| Sub-array excitation | $$w\_{m}=\frac{1}{\sqrt{M\_{sub}}}exp\left(j2π\left(m-1\right)\frac{d\_{v,sub}}{λ}sin\left(θ\_{subtilt}\right)\right)$$ |
| Sub-array radiation pattern | $$A\_{sub}\left(θ,φ\right)=A\_{E}\left(θ,φ\right)+10log\_{10}\left(\left|\sum\_{m=1}^{M\_{sub}}w\_{m}v\_{m}\right|^{2}\right)$$, where$$v\_{m}=exp\left(j2π\left(m-1\right)\frac{d\_{v,sub}}{λ}cos\left(θ\right)\right)$$ |
| Array excitation | $$w\_{m,n}=\frac{1}{\sqrt{MN}}exp\left(j2π\left(\left(m-1\right)\frac{d\_{v}}{λ}sin\left(θ\_{etilt}\right)-\left(n-1\right)\frac{d\_{h}}{λ}cos\left(θ\_{etilt}\right)sin\left(φ\_{escan}\right)\right)\right)$$Where *M* and *N* is corresponding to (Row × Column) in Table 4, row 1.6. |
| Composite array radiation pattern | $$A\_{A}\left(θ,φ\right)=A\_{sub}\left(θ,φ\right)+10log\_{10}\left(\left|\sum\_{m=1}^{M}\sum\_{n=1}^{N}w\_{m,n}v\_{m,n}\right|^{2}\right)$$, where$$v\_{m,n}=exp\left(j2π\left(\left(m-1\right)\frac{d\_{v}}{λ}cos\left(θ\right)+\left(n-1\right)\frac{d\_{h}}{λ}sin\left(θ\right)sin\left(φ\right)\right)\right)$$Where *M* and *N* is corresponding to (Row × Column) in Table 4, row 1.6. |

Considering base stations are optimized for various factors including performance, cost, and coverage, it is expected that sub array configurations are relevant where a set of physical antenna elements are combined to form a logical element. The model comprises of a basic element pattern which is then combined appropriately based on the equations to form the sub array pattern and the composite pattern. Since dual polarized elements are used in typical base stations, each polarization separately is considered in the models. The models are selected so that they are simple and representative to model BS performance with sufficient confidence. The element pattern is based on a simple gaussian beam which has a flat sidelobe level. The Gaussian pattern is sufficiently wide and cover most of the regions of interest, especially in the elevation domain. Thus, the extended antenna model with sub arrays is recommended to represent the beamforming capability of IMT base stations in considered frequency ranges.

**Table 4:** **Beamforming antenna characteristics for IMT in 14800 to 15350 MHz**

|  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- |
|  |  | **Macro suburban** | **Macro urban** | **Micro urban** | **Small cell indoor/Indoor urban** |
| **1** | **Base station Antenna Characteristics** |
| 1.1 | Antenna pattern  | Table 3 | N/A |
| 1.2 | Element gain (dBi) (Note 2) | 6.4 | 6.4 | 6.4 | 5 |
| 1.3 | Horizontal/vertical 3 dB beam width of single element (degree)  | 90º for H65º for V | 90º for H65º for V | 90º for H65º for V | 90º for H90º for V |
| 1.4 | Horizontal/vertical front‑to‑back ratio (dB) | 30 for both H/V | 30 for both H/V | 30 for both H/V | 30 for both H/V |
| 1.5 | Antenna polarization  | Linear ±45º polarized sub-array | Linear ±45º polarized sub-array | Linear ±45º polarized sub-array | Linear ±45º polarized sub-array |
| 1.6 | Antenna array configuration (Row × Column) (Note 4) | 16x24  | 16x24 | 16x24 | 4x4 |
| 1.7 | Horizontal/Vertical radiating sub-array or element spacing (Note 5) | 0.5 of wavelength for H, 2.8 of wavelength for V | 0.5 of wavelength for H, 2.8 of wavelength for V | 0.5 of wavelength for H, 2.8 of wavelength for V | 0.5 of wavelength for H, 0.5 of wavelength for V |
| 1.7a | Number of element rows in sub-array | 4 | 4 | 4 | N/A |
| 1.7b | Vertical element separation in sub-array ($d\_{v,sub}$) | 0.7 of wavelength for V | 0.7 of wavelength for V | 0.7 of wavelength for V | N/A |
| 1.7c | Pre-set sub-array down-tilt (degrees) (Note 6) | 3 | 3 | 3 | N/A |
| 1.8 | Array Ohmic loss (dB) (Note 2) | 2 | 2 | 2 | 2 |
| 1.9 | Conducted power (before Ohmic loss) per sub-array or element (dBm) (Note 3) | 17.2 | 17.2 | 7.2 | 8.0 |
| 1.10 | Base station horizontal coverage range (degrees) | ±60 | ±60 | ±60 | ±90 |
| 1.11 | Base station vertical coverage range (degrees) (Note 1) | 90-100 | 90-100 | 90-100 | 0-180 |
| 1.12 | Mechanical down-tilt (degrees) | 6 | 6 | 6 | N/A |
| 1.13 | Base station output power/sector (e.i.r.p.) (dBm) (Note 7) | 84.3 | 84.3 | 74.3 | 40.0 |

Note 1: The vertical coverage range is given in global coordinate system, i.e., 90° being at the horizon. This range includes the mechanical down-tilt given in row 1.12.

Note 2: The element gain in row 1.2 includes the loss given in row 1.8 and is per polarization.

Note 3: Conducted power values are per polarization. The conducted power per sub-array assumes 16 × 24 sub-arrays and 2 polarizations for the Macro Suburban, Macro Urban and Micro Urban cases; the conducted power per element assumes 4x4 elements for the Small cell indoor/ Indoor Urban case. This power is typical power, there is no upper limit for Wide Area Base station (For BS class definitions, see 3GPP TS 38.104 [1], § 4.4).

Note 4: 16 × 24 means there are 16 rows and 24 columns of radiating sub-arrays for Macro Suburban, Macro Urban and Micro Urban cases. 4x4 means there are 16 rows and 24 columns of radiating elements for Small cell indoor/ Indoor Urban case.

Note 5: For the case of 4 elements per sub-array, dv will be 2.8 wavelengths.

Note 6: The pre-set sub array down-tilt is a fixed design parameter for a base station. It is envisaged as a passive fixed (non-varying) electrical tilt within the sub-array elements.

Note 7: The base station e.i.r.p per sector is calculated as total power (including power from two orthogonal polarizations).

Note 8: Mechanical down-tilt is handled by a coordinate system transformation described in 3GPP TR 36.814 section A.2.1.6.2.

Note 9: $θ\_{etilt}$ and $φ\_{escan}$ is the BS array antenna beam steering direction used in Table 3, they should be set so that the beam steering direction is within the vertical and horizontal coverage ranges in row 1.11 and row 1.10, respectively.

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